

# CRITICAL CURRENT DENSITY, IRREVERSIBILITY LINE, AND FLUX CREEP ACTIVATION ENERGY IN SILVER-SHEATHED $\text{Bi}_2\text{Sr}_2\text{Ca}_2\text{Cu}_3\text{O}_x$ SUPERCONDUCTING TAPES

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**Abstract**--Transport data, magnetic hysteresis and flux creep activation energy experimental results are presented for silver-sheathed high- $T_c$   $\text{Bi}_2\text{Sr}_2\text{Ca}_2\text{Cu}_3\text{O}_x$  superconducting tapes. The 110 K superconducting phase was formed by lead doping in a Bi-Sr-Ca-Cu-O system. The transport critical current density was measured at 4.0 K to be  $0.7 \times 10^5$  A/cm<sup>2</sup> (the corresponding critical current is 74 A) at zero field and  $1.6 \times 10^4$  A/cm<sup>2</sup> at 12 T for Hllab. Excellent grain alignment in the a-b plane was achieved by a short-melting method, which considerably improved the critical current density and irreversibility line. Flux creep activation energy as a function of current is obtained based on the magnetic relaxation measurements.

## I. INTRODUCTION

Large-scale application of high- $T_c$  superconductivity depends on the successful production of long wires with high current-carrying capability, mechanical flexibility, and chemical stability. The metal-sheathed powder-in-tube technique has proved successful for making long high- $T_c$  superconductor wires that can carry high critical current densities [1-5]. Specifically, Bi-based superconducting tapes that can carry critical current densities greater than  $1 \times 10^5$  A/cm<sup>2</sup> in high magnetic field ( $> 20$  T) at 4.2 K have been developed [5]. In this paper, we report on the critical current density and irreversibility data for silver-sheathed Bi-Pb-Sr-Ca-Cu-O tapes processed by a novel method. We discuss the possible relationship between the critical current and the microstructure of the tapes.

## II. EXPERIMENTAL PROCEDURE

The processing method for making the silver-sheathed Bi-Pb-Sr-Ca-Cu-O tapes was previously reported by Dou et al. [1]. The superconducting powders were made by a freeze-drying technique [1]. The solution of  $\text{Bi}_2\text{O}_3$  in nitric acid was mixed with  $\text{Pb}(\text{NO}_3)_2$ ,  $\text{Ca}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$ ,  $\text{Sr}(\text{NO}_3)_2$ , and  $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$  in distilled water in the ratios Bi : Pb : Sr : Ca : Cu = 1.6 : 0.4 : 1.6 : 2 : 3. The solutions were then quickly frozen by spraying into a liquid nitrogen bath. The frozen mixtures of the nitrates were placed in a freeze drier and

dried under vacuum for 48 h. The dried powders were calcined in air at 830°C for 10 h. The calcined powders were then pressed into pellets and sintered at 850°C for 20 h. The sintered pellets were powdered and poured into a silver tube of 10 mm outside diameter and 8 mm inside diameter. The silver tube was then rolled into tapes 0.1 mm thick and ~2-3 mm wide. Two types of heat treatment were used in this study. Sample 1 was heat treated at ~820°C for 150 h in a mixture of oxygen and nitrogen with varying  $\text{O}_2$  partial pressure; the heat treatment was repeated twice to optimize the grain alignment. Sample 2 was heat treated at ~830°C for 70 h in a similar atmosphere; in addition, it underwent a partial melting at 860°C for 20-30 min. The detailed processing procedure for partial melting of Sample 2 can be found elsewhere [2].

The transport critical current density,  $J_c$ , of the silver-sheathed tapes was measured at 4.0 K up to 12 T and 76 K up to 1 T. The measurements were performed by using a standard four-probe method with a voltage criterion of 1  $\mu\text{V}/\text{cm}$ . The direction of the transport current was perpendicular to the applied field. For comparison, we also measured magnetization critical current density in a wide temperature regime using a vibrating sample magnetometer. By applying the Bean critical state model [6] we calculated the magnetization  $J_c$  (A/cm<sup>2</sup>) using the formula  $\Delta M = a_2 J_c (1 - a_2/3a_1)/20$ , where  $\Delta M$  is the magnetic hysteresis difference in emu/cm<sup>3</sup>, and  $2a_1 \times 2a_2$  is the cross-sectional area of the sample ( $a_1 > a_2$ ).

## III. RESULTS AND DISCUSSION

In agreement with most of the previously reported transport data, the high  $J_c$  value of Sample 1 remained approximately the same ( $> 1 \times 10^4$  A/cm<sup>2</sup>) as the field reached 12 T at 4.0 K for both Hllab and Hllc (Fig. 1). However, the  $J_c$  (Hllab) was about 20% higher than the  $J_c$  (Hllc) at 12 T and  $T = 4.0$  K. It should be pointed out that the total critical current at 4.0 K and zero field reached a maximum value of 74 A [3].

We found that the texturing in the silver-sheathed tapes was greatly enhanced by the short-melting process. As can be

seen in Fig. 2, Sample 2 has a higher degree of texture compared with the previously obtained microstructure [3]. Although some degree of texturing can be obtained by extended sintering (150 h at 820°C), the short-melting process at partial melting temperature is required to further improve the grain alignment for achieving an optimized critical current density.

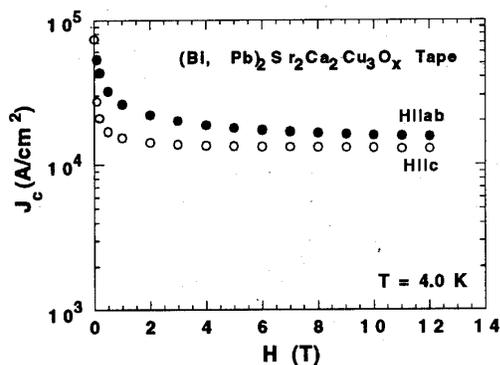


Fig. 1. Transport  $J_C$  vs.  $H$  at at 4.0 K for sample 1.

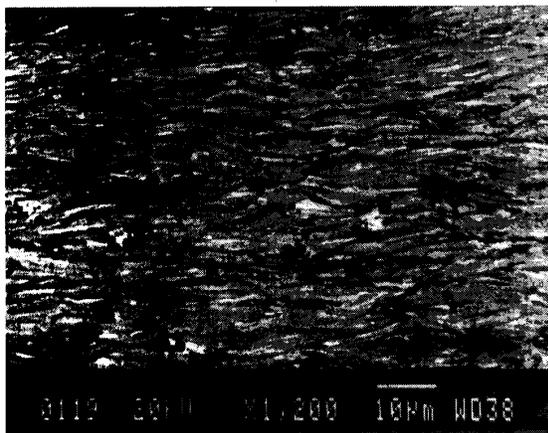


Fig. 2. Scanning electron microscopy photograph showing highly  $c$  axis-oriented grains in a tape processed by short-melting method.

The magnetic hysteresis curves were obtained from 4.2 K to 90 K for the applied fields up to 5 T for Hllc. Figure 3 shows the temperature dependence of the  $J_C$  at 0.5 T for Samples 1 and 2. As can be seen, the  $J_C$  of sample 2 is considerably increased relative to that of sample 1 with increasing temperature, particularly in the high temperature range. However, in the temperature range below 50 K, the  $J_C$  value of sample 2 is lower than that of sample 1.

It has been well reported that flux-creep effects are strong in the bismuth-based system and that the "irreversibility line" lies in the low regions of temperature and field compared with those of the  $YBa_2Cu_3O_x$  compound.

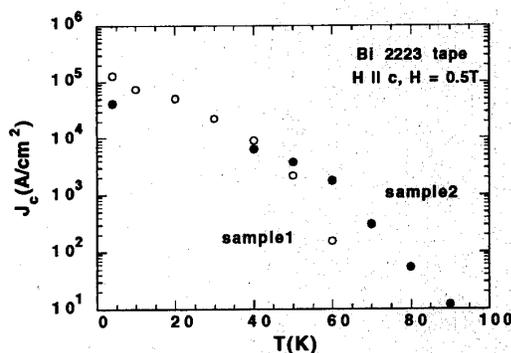


Fig. 3. Magnetization  $J_C$  vs. temperature,  $T$ , at 0.5 T for sample 1 and 2.

Figure 4 shows the irreversibility lines of samples 1 and 2. We have defined the irreversibility line as the point where the hysteresis loop closes. A similar effect to the temperature dependence of  $J_C$  shown in Fig. 3 is observed. It has been found that partial melting generates a high density of dislocations in the superconducting phase and that these dislocations can act as pinning centers [2]. Moreover, as with  $J_C$ , the shift of the irreversibility line in sample 2 is more pronounced at high temperatures. Below 10 K and at high fields, the irreversibility lines of samples 1 and 2 are located in the nearby regions.

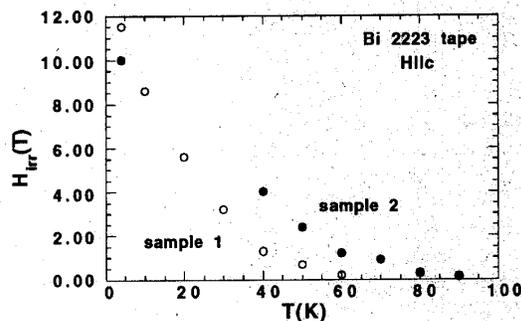


Fig. 4. Irreversibility lines determined based on the magnetic hysteresis data for samples 1 and 2.

It is not clear why, at high temperatures, the  $J_C$ 's and the irreversibility line for sample 2 is higher than sample 1. A possible interpretation is that the flux pinning increases with temperature as a result of the short-melting method, although the pinning mechanism is still to be identified. On the other hand, the difference in anisotropy of  $J_C$  at 4.0 K and 77 K suggests that pinning by Cu-O planes is not important at low temperatures, where the superconducting system is

more uniform. As observed in Ref. 3 and shown in Fig. 1, the  $J_c$  is not much different for both Hllc and Hllab, while a large difference in  $J_c$  is observed at 77 K for these configurations.

We consider here that the effective activation energy,  $U$ , is a function of  $J$ , which is temperature and field dependent [7]. We expand the effective activation energy  $U(J)$  about some current  $J_0$  at time  $t_0$  to obtain

$$U(J) = U(J_0) + [\partial U/\partial J]_0(J - J_0) + (1/2)[\partial^2 U/\partial J^2]_0(J - J_0)^2 + \dots \\ \sim U(J_0) + \alpha (J - J_0) + (1/2)\beta (J - J_0)^2 + \dots \quad (1)$$

where  $\alpha = [\partial U/\partial J]_0$  and  $\beta = [\partial^2 U/\partial J^2]_0$ .

Considering the second-order term and assuming that the preexponential factor  $A$  is constant in the temperature range considered, one obtains that

$$J(t) = J_0 + (kT/\alpha) \ln(t/t_0) - (k^2 T^2 \beta / 2\alpha^3) \ln^2(t/t_0). \quad (2)$$

Using Bean's model, one can rewrite above equation as

$$M(t) = M_0 + a \ln(t/t_0) + b \ln^2(t/t_0), \quad (3)$$

where  $a = (kT)[\partial M/\partial U]_0$  and  $b = -(k^2 T^2 / 2)[\partial^2 U/\partial M^2]_0 [\partial M/\partial U]_0^3$ . Experimentally, one can determine the constants  $a$  and  $b$  from the magnetic relaxation measurements and use them to calculate  $\alpha$  and  $\beta$ . Substituting  $\alpha$  and  $\beta$  into Equation (1), a smooth U-J curve can be obtained. This method is equivalent to that developed by Maley et al. [8]. Figure 5 shows the U-J relationship for sample 1. As can be seen, at large driving force,  $U$  varies gradually while a rapid increase is observed as  $J$  is reduced to a small level. We found that this behavior is typical for most of the type-II superconductors including A-15 Nb<sub>3</sub>Sn.

In conclusion, we have found that the  $J_c$  and the irreversibility line are considerably enhanced in silver-sheathed Bi-based superconducting tapes by employing a short-melting method developed previously. The flux-pinning strength has been found to increase with temperature, resulting in more pronounced enhancement of  $J_c$  in the partially melted tape at high temperatures. The pinning mechanism associated with the enhancement of the  $J_c$  and the irreversibility line in sample 2 is under investigation. We have obtained the flux-creep activation energy of the silver-sheathed tape based on magnetic relaxation data.

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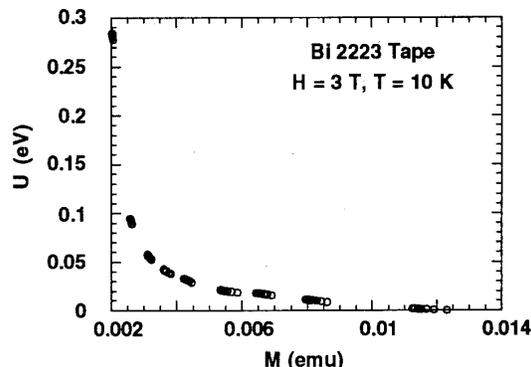


Fig. 5. U vs. M curve for Sample 1.

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